

The following excerpt are pages from the North American Product Technical Guide, Volume 2: Anchor Fastening, Edition 21.

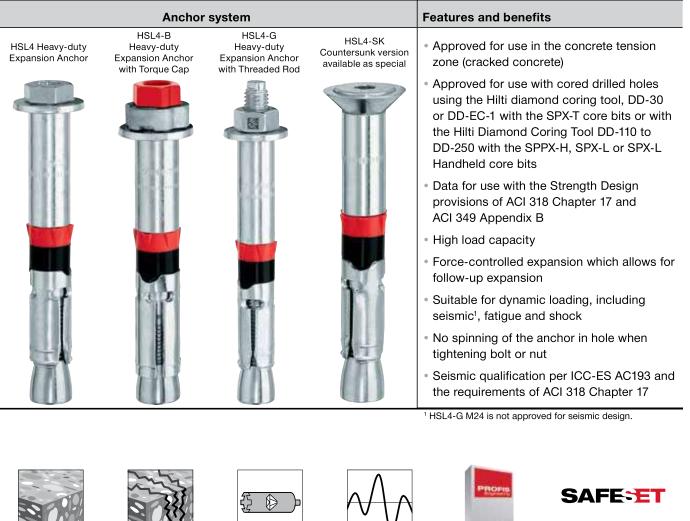
Please refer to the publication in its entirety for complete details on this product including data development, product specifications, general suitability, installation, corrosion and spacing and edge distance guidelines. US&CA: <u>https://submittals.us.hilti.com/PTGVol2/</u>

To consult directly with a team member regarding our anchor fastening products, contact Hilti's team of technical support specialists between the hours of 7:00am – 6:00pm CST. US: 877-749-6337 or <u>HNATechnicalServices@hilti.com</u> CA: 1-800-363-4458, ext. 6 or <u>CATechnicalServices@hilti.com</u>

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# 3.3.2 HSL4 HEAVY-DUTY EXPANSION ANCHORS

# PRODUCT DESCRIPTION



Uncracked concrete

Cracked concrete

Diamond cored holes for cracked and uncracked concrete

Seismic Design

Categories

A-F

Profis Anchor design software

Hollow Drill Bit

3.3.2

CC-ES (International Code Council)	ESR-4386 in concrete per ACI 318 Ch. 17 / ACI 355.2/ ICC-ES AC193
European Technical Approval	ETA-19/0556
City of Los Angeles	2020 LABC Supplement (within ESR-4386)
Nuclear Quality Assurance	Qualified under NQA-1 Nuclear Quality Program





## MATERIAL SPECIFICATIONS

Carbon steel bolt or threaded rod for HSL4, HSL4-G, HSL4-B and HSL4-SK conform to the steel strength requirements of ISO 898-1, grade 8 .8,  $f_{ya}$  > 93 ksi,  $f_{uta}$  > 116 ksi.

Nut, washer, expansion cone, expansion sleeve and spacing sleeve are all made of carbon steel.

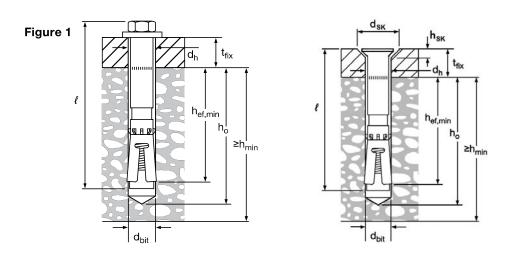
Collapsible sleeve is made from acetal polyoxymethylene (POM) resin and thermoplastic elastomer (TPE).

## INSTALLATION PARAMETERS

## Table 1 — HSL4 Specifications

Details	Details						HS	SL4 ar	nchor t	hread c	liamet	ər				
Dotailo			Ν	18	М	10		M12			M16		М	20	M	24
Nominal drill bit diameter <sup>1</sup>	d <sub>bit</sub>	mm	1	2	1	5		18			24		2	8	3	2
Minimum concrete thick- ness	h <sub>min</sub>	mm (in.)							See t	able 5			1			
Minimum hole depth	h <sub>。</sub>	mm (in.)	-	80 1/8)	9 (3- <sup>-</sup>	-	(	105 4-1/8)	)		125 (4-7/8)			55 1/8)	18 (7- <sup>-</sup>	
Effective minimum embe- dment	h <sub>ef,min</sub>	mm (in.)	60 (2-3/8)		7 (2-3	0 3/4)	(	80 3-1/8)	)		100 (3-7/8)			25 7/8)	15 (5-7	
Fixture hole diameter	d <sub>h</sub>	mm (in.)	14         17         20         26         31           (9/16)         (11/16)         (13/16)         (1)         (1-1/4)		3 (1-3	-										
Maximum thickness of part fastened HSL4, HSL4-B	t <sub>fix</sub>	mm (in.)	20 (3/4)	20 40		40 (1-1/2)	5 (1/5)	25 (1)	50 (2)	10 (2/5)	25 (1)	50 (2)	30 (1-1/8)	60 (2-1/4)	30 (1-1/8)	60 (2-1/4)
Maximum thickness of part fastened HSL4-G	t <sub>fix</sub>	mm (in.)		:0 /4)	20 (3/4)	100 (4)	25 (1)		50 (2)	25 (1)		50 (2)	30 (1-1/8)	60 (2-1/4)		
Washer diameter	d <sub>w</sub>	mm (in.)		:0 /4)	2 (*	-	(	30 1-1/8)	)	(	40 1-9/16	)		-5 3/4)	5 (2	
Installation torque HSL4	T <sub>inst</sub>	Nm (ft-lb)		5 1)	2 (1	-		60 (44)			75 (55)		-	45 07)	21 (15	
Installation torque HSL4-G	T <sub>inst</sub>	Nm (ft-lb)		:0 5)	2 (2			60 (44)			70 (52)		1( (7	05 77)	18 (13	
Installation torque HSL4-SK	T <sub>inst</sub>	Nm (ft-lb)		25 8)	3 (2			65 (48)			_			_	-	-
Wrench size HSL4, HSL4-G	sw	mm	1	3	1	7		19			24		3	0	3	6
Wrench size HSL4-B	SW	mm	-	-	-	_		24			30		3	6	4	1
Wrench size HSL4-SK	SW	mm	Į	5	e	3		8			-			-	-	-
Diameter of countersunk hole HSL4-SK	d <sub>sk</sub>	mm	22	2.5	25	5.5		32.9			-			-	-	-

<sup>1</sup> Use metric bits only.



## **DESIGN DATA IN CONCRETE PER ACI 318**

## ACI 318 Chapter 17 Design

The load values contained in this section are Hilti Simplified Design Tables. The load tables in this section were developed using the Strength Design parameters and variables of ESR-4386 and the equations within ACI 318 Chapter 17. For a detailed explanation of the Hilti Simplified Design Tables, refer to section 3.1.8 of the North American Product Technical Guide, Volume 2: Anchor Fastening Technical Guide, Edition 21 (PTG Ed. 21). Data tables from ESR-4386 are not contained in this section but can be found at www.icc-es.org or at www.hilti.com.

#### Table 2 — Hilti HSL4 design strength with concrete / pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>

			Tensio	n - φN <sub>n</sub>			Shear	r - φV <sub>n</sub>	
Nominal	Effective	f'₀ =	f' <sub>c</sub> =	f' <sub>c</sub> =	f' <sub>c</sub> =	f' <sub>c</sub> =	f'c =	f'c =	f' <sub>c</sub> =
anchor	embed.	2,500 psi	3,000 psi	4,000 psi	6,000 psi	2,500 psi	3,000 psi	4,000 psi	6,000 psi
diameter	mm (in.)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)
M8	60	2,735	2,995	3,455	4,235	3,050	3,340	3,860	4,725
	(2.4)	(12.2)	(13.3)	(15.4)	(18.8)	(13.6)	(14.9)	(17.2)	(21.0)
M10	70	3,570	3,910	4,515	5,530	7,685	8,420	9,720	11,905
	(2.8)	(15.9)	(17.4)	(20.1)	(24.6)	(34.2)	(37.5)	(43.2)	(53.0)
M12	80	4,360	4,775	5,515	6,755	9,390	10,285	11,880	14,550
	(3.2)	(19.4)	(21.2)	(24.5)	(30.0)	(41.8)	(45.7)	(52.8)	(64.7)
M16	100	6,095	6,675	7,705	9,440	13,125	14,375	16,600	20,330
	(3.9)	(27.1)	(29.7)	(34.3)	(42.0)	(58.4)	(63.9)	(73.8)	(90.4)
M20	125	8,515	9,330	10,770	13,190	18,340	20,090	23,200	28,415
	(4.9)	(37.9)	(41.5)	(47.9)	(58.7)	(81.6)	(89.4)	(103.2)	(126.4)
M24	150	11,195	12,260	14,160	17,340	24,110	26,410	30,495	37,350
	(5.9)	(49.8)	(54.5)	(63.0)	(77.1)	(107.2)	(117.5)	(135.6)	(166.1)

			Tensio	n - φN <sub>n</sub>			Shear	- φV <sub>n</sub>	
Nominal	Effective	f'c =	f' <sub>c</sub> =	f' <sub>c</sub> =	f' <sub>c</sub> =	f' <sub>c</sub> =	f' <sub>c</sub> =	f' <sub>c</sub> =	f' <sub>c</sub> =
anchor	embed.	2,500 psi	3,000 psi	4,000 psi	6,000 psi	2,500 psi	3,000 psi	4,000 psi	6,000 psi
diameter	mm (in.)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)	Ib (kN)
	60	1,825	2,000	2,310	2,830	2,160	2,365	2,730	3,345
M8	(2.4)	(8.1)	(8.9)	(10.3)	(12.6)	(9.6)	(10.5)	(12.1)	(14.9)
M10	70	2,920	3,200	3,695	4,525	7,685	8,420	9,720	11,905
	(2.8)	(13.0)	(14.2)	(16.4)	(20.1)	(34.2)	(3 .5)	(43.2)	(53.0)
M12	80	4,360	4,775	5,515	6,755	9,390	10,285	11,880	14,550
	(3.2)	(19.4)	(21.2)	(24.5)	(30.0)	(41.8)	(45.7)	(52.8)	(64.7)
M16	100	6,095	6,675	7,705	9,440	13,125	14,375	16,600	20,330
	(3.9)	(27.1)	(29.7)	(34.3)	(42.0)	(58.4)	(63.9)	(73.8)	(90.4)
M20	125	8,515	9,330	10,770	13,190	18,340	20,090	23,200	28,415
	(4.9)	(37.9)	(41.5)	(47.9)	(58.7)	(81.6)	(89.4)	(103.2)	(126.4)
M24 <sup>5</sup>	150	11,195	12,260	14,160	17,340	24,110	26,410	30,495	37,350
	(5 .9)	(49.8)	(54.5)	(63.0)	(77.1)	(107.2)	(117.5)	(135.6)	(166.1)

1 See PTG Ed. 21 section 3.1.8 to convert design strength value to ASD value.

Linear interpolation between concrete compressive strengths is not permitted.
 Apply spacing, edge distance, and concrete thickness factors in tables 5 to 8 as necessary. Compare to the steel values in table 4. The lesser of the values is to be used for the design.

Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: for sand-lightweight,  $\lambda_a = 0.68$ ; for all-lightweight,  $\lambda_a = 0.60$ .

Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For all seismic tension loads for all other anchors, multiply cracked concrete tabular 5

values in tension only by the following reduction factors: M24 -  $\alpha_{N,seis}$  = 0 .62. HSL4-G M24 is not approved for seismic design.

All other sizes – av<sub>uses</sub> = 0.75 No reduction needed for seismic shear. See PTG Ed. 21 section 3.1.8 for additional information on seismic applications.

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## Table 4 — Steel strength for Hilti HSL4 anchors<sup>1,2</sup>

	HS	L4, HSL4-B, HSL4-	-SK		HSL4-G	
Nominal anchor diameter	Tensile³ φN <sub>sa</sub> Ib (kN)	Shear⁴ φV <sub>sa</sub> Ib (kN)	Seismic shear⁵ ¢V <sub>sa,eq</sub> Ib (kN)	Tensile <sup>3</sup> φN <sub>sa</sub> Ib (kN)	Shear <sup>4</sup>	Seismic shear⁵ ¢V <sub>sa.eq</sub> Ib (kN)
M8	4,960	4,705	2,995	4,960	3,945	2,455
	(22 .1)	(20 .9)	(13 .3)	(22 .1)	(17 .5)	(10 .9)
M10	7,830	6,650	5,495	7,830	5,450	4,500
	(34 .8)	(29 .6)	(24 .4)	(34 .8)	(24 .2)	(20 .0)
M12	11,395	9,570	7,730	11,395	7,905	6,385
	(50 .7)	(42 .6)	(34 .4)	(50 .7)	(35 .2)	(28 .4)
M16	21,140	17,360	16,115	21,140	14,745	13,690
	(94 .0)	(77 .2)	(71 .7)	(94 .0)	(65 .6)	(60 .9)
M20	33,060	25,690	18,940	33,060	21,555	15,900
	(147 .1)	(114 .3)	(84 .2)	(147 .1)	(95 .9)	(70 .7)
M24	47,590 (211 .7)	29,870 (132 .9)	24,810 (110 .4)	47,590 (211 .7)	28,060 (124 .8)	n/a

1 See PTG Ed. 21 section 3.1.8 to convert design strength value to ASD value.
2 Hilti HSL4 Carbon Steel anchors are to be considered ductile steel elements.
3 Tensile φN<sub>sa</sub> = φ<sub>Ase,N</sub>f<sub>ua</sub> as noted in ACI 318 Chapter 17
4 Shear values determined by static shear tests with φV<sub>sa</sub> ≤ φ 0.60 A<sub>se,V</sub> f<sub>uta</sub> as noted in ACI 318 Chapter 17
5 Seismic shear values determined by seismic shear tests with φV<sub>sa</sub> ≤ φ 0.60 A<sub>se,V</sub> f<sub>uta</sub> as noted in ACI 318 Chapter 17
5 Seismic shear values determined by seismic shear tests with φV<sub>sa</sub> ≤ φ 0.60 A<sub>se,V</sub> f<sub>uta</sub> as noted in ACI 318 Chapter 17
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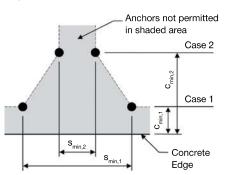
							Nominal and	hor diameter		
Condition	Dim	nensional parameter	Symbol	Units	M8	M10	M12	M16	M20	M24
	Minimum c	oncrete thickness	h <sub>min</sub>	in. (mm)	4-3/4 (120)	5-1/2 (140)	6-1/4 (160)	7-7/8 (200)	9-7/8 (250)	11-7/8 (300)
	Critical edg	je distance	C <sub>ac</sub>	in. (mm)	4-3/8 (110)	4-3/8 (110)	4-3/4 (120)	5-7/8 (150)	8-7/8 (225)	8-7/8 (225)
А	Case 1	Minimum edge distance	C <sub>min,1</sub>	in. (mm)	2-3/8 (60)	2-3/4 (70)	3-1/2 (90)	4-3/4 (120)	5 (125)	5-7/8 (150)
A	Case 1	Minimum anchor spacing	S <sub>min,1</sub>	in. (mm)	5-1/2 (140)	9-1/2 (240)	11 (280)	12-5/8 (320)	13-3/4 (350)	11-7/8 (300)
	Case 2	Minimum edge distance	C <sub>min,2</sub>	in. (mm)	3-3/8 (85)	5 (125)	6-1/8 (155)	7-7/8 (200)	8-1/4 (210)	8-1/4 (210)
	Case 2	Minimum anchor spacing	S <sub>min,2</sub>	in. (mm)	2-3/8 (60)	2-3/4 (70)	3-1/8 (80)	4 (100)	5 (125)	5-7/8 (150)
	Minimum c	oncrete thickness	h <sub>min</sub>	in. (mm)	4-3/8 (110)	4-3/4 (120)	5-3/8 (135)	6-1/4 (160)	7-1/2 (190)	8-7/8 (225)
	Critical edg	le distance	C <sub>ac</sub>	in. (mm)	5-7/8 (150)	6-7/8 (175)	7-7/8 (200)	9-7/8 (250)	12-3/8 (312 .5)	14-3/4 (375)
В	Case 1	Minimum edge distance	C <sub>min,1</sub>	in. (mm)	2-3/8 (60)	3-1/2 (90)	4-3/8 (110)	6-1/4 (160)	7-7/8 (200)	8-7/8 (225)
В	Case I	Minimum anchor spacing	S <sub>min,1</sub>	in. (mm)	7 (180)	10-1/4 (260)	12-5/8 (320)	15 (380)	15-3/4 (400)	15 (380)
	Case 2	Minimum edge distance	C <sub>min,2</sub>	in. (mm)	4 (100)	6-1/4 (160)	7-7/8 (200)	10-5/8 (270)	11-7/8 (300)	12-5/8 (320)
	Case 2	Minimum anchor spacing	S <sub>min,2</sub>	in. (mm)	2-3/8 (60)	2-3/4 (70)	3-1/8 (80)	4 (100)	5 (125)	5-7/8 (150)

Table 5 – Edge distance, spacing and member thickness requirements<sup>1</sup>

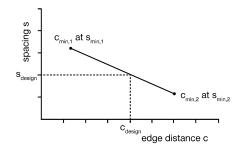
1 Linear interpolation is permitted to establish an edge distance and spacing combination between Case 1 and Case 2. Linear interpolation for a specific edge distance c, where  $c_{min,1} < c < c_{min,2}$  will determine the permissible spacing s as follows:

$$S \geq S_{\min,2} + \frac{\left(S_{\min,1} - S_{\min,2}\right)}{\left(C_{\min,1} - C_{\min,2}\right)} \left(C - C_{\min,2}\right)$$

Figure 2



For a specific edge distance, the permitted spacing is calculated as follows:





	, M10 and M Incracked co			tension $f_{\rm AN}$			ge dista or in ter $f_{_{\rm RN}}$			bing fac shear <sup>3</sup> f <sub>AV</sub>		Точ	Edge $\downarrow$ ward ec $f_{\rm RV}$		nce in s II to a	hear nd awa edge $f_{_{\rm RV}}$	y from		rete thic factor n shear $f_{_{\rm HV}}$	
	Nominal d	ia.	M8	M10	M12	M8	M10	M12	M8	M10	M12	M8	M10	M12	M8	M10	M12	M8	M10	M12
I	Effective	in.	2.38	2.76	3.15	2.36	2.76	3.15	2.38	2.76	3.15	2.38	2.76	3.15	2.38	2.76	3.15	2.38	2.76	3.15
emb	pedment h <sub>ef</sub>	(mm)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)
	2-3/8	(60)	0.67	n/a	n/a	0.45	n/a	n/a	0.58	n/a	n/a	0.32	n/a	n/a	0.45	n/a	n/a	n/a	n/a	n/a
	2-1/2	(64)	0.68	n/a	n/a	0.47	n/a	n/a	0.58	n/a	n/a	0.35	n/a	n/a	0.47	n/a	n/a	n/a	n/a	n/a
Ê	2-3/4	(70)	0.69	0.67	n/a	0.50	0.45	n/a	0.59	0.55	n/a	0.40	0.18	n/a	0.50	0.36	n/a	n/a	n/a	n/a
(mm)	3	(76)	0.71	0.68	n/a	0.53	0.48	n/a	0.60	0.56	n/a	0.46	0.20	n/a	0.53	0.41	n/a	n/a	n/a	n/a
.⊑	3-1/8	(79)	0.72	0.69	0.67	0.55	0.49	n/a	0.60	0.56	0.56	0.49	0.22	n/a	0.55	0.44	n/a	n/a	n/a	n/a
(j)	3-1/2	(89)	0.75	0.71	0.69	0.60	0.53	0.48	0.62	0.57	0.56	0.58	0.26	0.23	0.60	0.52	0.46	n/a	n/a	n/a
ss (	4	(102)	0.78	0.74	0.71	0.68	0.59	0.53	0.63	0.58	0.57	0.71	0.32	0.28	0.71	0.59	0.53	n/a	n/a	n/a
٨ne	4-3/8	(111)	0.81	0.76	0.73	0.74	0.64	0.56	0.65	0.58	0.58	0.81	0.36	0.32	0.81	0.64	0.56	0.76	n/a	n/a
ihicl	4-1/2	(114)	0.82	0.77	0.74	0.77	0.65	0.58	0.65	0.59	0.58	0.85	0.38	0.34	0.85	0.65	0.58	0.77	n/a	n/a
ete t	4-3/4	(121)	0.84	0.79	0.75	0.81	0.69	0.60	0.66	0.59	0.59	0.92	0.41	0.37	0.92	0.69	0.60	0.79	0.61	n/a
lore	5	(127)	0.85	0.80	0.76	0.85	0.73	0.63	0.67	0.60	0.59	0.99	0.44	0.40	0.99	0.73	0.63	0.81	0.62	n/a
cor	5-3/8	(137)	0.88	0.83	0.78	0.91	0.78	0.68	0.68	0.60	0.60	1.00	0.49	0.44	1.00	0.78	0.68	0.84	0.64	0.62
( <sup>e</sup> )	6	(152)	0.92	0.86	0.82	1.00	0.87	0.76	0.70	0.62	0.61		0.58	0.52		0.87	0.76	0.89	0.68	0.66
9) 9)	7	(178)	0.99	0.92	0.87		1.00	0.89	0.73	0.64	0.63		0.73	0.65		1.00	0.89	0.96	0.73	0.71
anc	8	(203)	1.00	0.98	0.92			1.00	0.77	0.65	0.64		0.89	0.80			1.00	1.00	0.79	0.76
distance ( $c_a$ ) / concrete thickness	9	(229)	1	1.00	0.98				0.80	0.67	0.66		1.00	0.95					0.83	0.80
/ edge	10	(254)	1	1.00	1.00				.083	0.69	0.68			1.00					0.88	0.85
/ eq	12	(305)		1.00	1.00				0.90	0.73	0.72								0.96	0.93
(s)	14	(356)			1.00				0.96	0.77	0.75								1.00	1.00
ing	16	(406)	1						1.00	0.81	0.79									
Spacing (s)	18	(457)								0.85	0.82									
Ś	20	(508)								0.89	0.86									
	24	(610)								0.96	0.93									
	> 30	(762)								1.00	1.00									

## Table 6 — Load adjustment factors for M8, M10, and M12 Hilti HSL4 anchors in uncracked concrete<sup>1,2</sup>

## Table 7 — Load adjustment factors for M8, M10, and M12 Hilti HSL4 anchors in cracked concrete<sup>1,2</sup>

								<u>,</u>	_				Edg	e distar	nce in sl	near		Conc	ete thic	kness
M8	, M10 and M1	12 HSL4		tension			ge dista or in ter			shear 3	tor in				II to a	nd awa	y from		factor	
	cracked cond	orete		$f_{AN}$		Tacto	$f_{\rm RN}$	ision		f <sub>AV</sub>		Tov	ward ec	lge		edge		i	n shear	4
				JAN			J RN			JAV			$f_{\scriptscriptstyleRV}$	-		f <sub>RV</sub>			$f_{HV}$	
	Nominal di	ia.	M8	M10	M12	M8	M10	M12	M8	M10	M12	M8	M10	M12	M8	M10	M12	M8	M10	M12
	Effective	in.	2.38	2.76	3.15	2.36	2.76	3.15	2.38	2.76	3.15	2.38	2.76	3.15	2.38	2.76	3.15	2.38	2.76	3.15
emb	pedment h <sub>ef</sub>	(mm)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)	(60)	(70)	(80)
	2-3/8	(60)	0.67	n/a	n/a	0.75	n/a	n/a	0.58	n/a	n/a	0.33	n/a	n/a	0.65	n/a	n/a	n/a	n/a	n/a
	2-1/2	(64)	0.68	n/a	n/a	0.78	n/a	n/a	0.58	n/a	n/a	0.35	n/a	n/a	0.71	n/a	n/a	n/a	n/a	n/a
Ê	2-3/4	(70)	0.69	0.67	n/a	0.83	0.75	n/a	0.59	0.54	n/a	0.41	0.13	n/a	0.82	0.28	n/a	n/a	n/a	n/a
- in (mm)	3	(76)	0.71	0.68	n/a	0.88	0.79	n/a	0.60	0.55	n/a	0.46	0.15	n/a	0.88	0.29	n/a	n/a	n/a	n/a
.⊆	3-1/8	(79)	0.72	0.69	0.67	0.91	0.81	n/a	0.60	0.55	0.54	0.49	0.16	n/a	0.91	0.31	n/a	n/a	n/a	n/a
	3-1/2	(89)	0.75	0.71	0.69	0.99	0.88	0.80	0.62	0.55	0.55	0.59	0.18	0.17	0.99	0.37	0.33	n/a	n/a	n/a
ss (	4	(102)	0.78	0.74	0.71	1.00	0.97	0.88	0.63	0.56	0.56	0.72	0.23	0.20	1.00	0.45	0.40	n/a	n/a	n/a
edge distance ( $c_{\rm a}$ ) / concrete thickness (h),	4-3/8	(111)	0.81	0.76	0.73		1.00	0.94	0.65	0.57	0.56	0.82	0.26	0.23		0.51	0.46	0.76	n/a	n/a
hic	4-1/2	(114)	0.82	0.77	0.74		1.00	0.96	0.65	0.57	0.56	0.85	0.27	0.24		0.54	0.48	0.77	n/a	n/a
te t	4-3/4	(121)	0.84	0.79	0.75		1.00	1.00	0.66	0.57	0.57	0.93	0.29	0.26		0.58	0.52	0.80	0.54	n/a
lore	5	(127)	0.85	0.80	0.76		1.00	1.00	0.67	0.58	0.57	1.00	0.31	0.28		0.63	0.56	0.82	0.56	n/a
cor	5-3/8	(137)	0.88	0.83	0.78		1.00	1.00	0.68	0.58	0.58		0.35	0.31		0.70	0.63	0.85	0.58	0.56
/ (°:	6	(152)	0.92	0.86	0.82		1.00	1.00	0.70	0.59	0.59		0.41	0.37		0.83	0.74	0.89	0.61	0.59
e (c	7	(178)	0.99	0.92	0.87		1.00	1.00	0.73	0.61	0.60		0.52	0.47		1.00	0.93	0.97	0.66	0.63
anc	8	(203)	1.00	0.98	0.92			1.00	0.77	0.62	0.61		0.64	0.57			1.00	1.00	0.70	0.68
dist	9	(229)		1.00	0.98				0.80	0.67	0.63		1.00	0.68					0.74	0.72
ge i	10	(254)		1.00	1.00		İ		.083	0.65	0.64		0.89	0.80					0.79	0.76
/ ed	12	(305)		1.00	1.00				0.90	0.69	0.67		1.00	1.00					0.86	0.83
(s)	14	(356)			1.00				0.96	0.72	0.70								1.93	0.90
ing	16	(406)			İ 👘		1		1.00	0.75	0.73						1		0.99	0.96
Spacing (s)	18	(457)								0.78	0.76								1.00	1.00
S	20	(508)								0.81	0.86									
	24	(610)								0.87	0.84									
	> 30	(762)								0.96	0.93									

1. Linear interpolation not permitted.

Linear interpolation not permitted.
 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Engineering software or perform anchor calculation using design equations from ACI 318 Chapter 17.
 Spacing factor reduction in shear, *f<sub>HV</sub>*, assumes an influence of a nearby edge. If no edge exists, then *f<sub>AV</sub>* = *f<sub>AN</sub>*.
 Concrete thickness reduction factor value is in a shaded cell, it may not be permitted if both edge and spacing are less than "critical" distances. Check table 5 and figure 2 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. For the HSL4-SH M8, M10 and M12 diameters, the minimum slab thickness must be increased by Emm (2166 m).

increased by 5 mm (3/16-in.).

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			0					,	0				Edg	e distar	nce in s			Concr	ete thic	kness
	, M20 and N			ing fact			ge dista or in ter			ing fact shear <sup>3</sup>	tor in		1		II to a	nd awa	y from	1	factor	
ur	ncracked co	ncrete		$f_{AN}$			$f_{\rm RN}$	151011		f <sub>AV</sub>		Τον	ward ec	lge		edge		ii	n shear	4
													f <sub>RV</sub>			f <sub>RV</sub>			f <sub>HV</sub>	
	Nominal d	ia.	M16	M20	M24	M16	M20	M24	M16	M20	M24	M16	M20	M24	M16	M20	M24	M16	M20	M24
	ffective	in.	3.948	4.92	5.91	3.948	4.92	5.91	3.948	4.92	5.91	3.948	4.92	5.91	3.948	4.92			4.92	5.91
emb	edment h <sub>ef</sub>	(mm)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)
	4	(102)	0.67	n/a	n/a	n/a	n/a	n/a	0.56	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a
	4-1/2	(114)	0.69	n/a	n/a	n/a	n/a	n/a	0.57	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a
Ê	4-3/4	(121)	0.70	n/a	n/a	0.51	n/a	n/a	0.58	n/a	n/a	0.30	n/a	n/a	0.51	n/a	n/a	n/a	n/a	n/a
- in (mm)	5	(127)	0.71	0.67	n/a	0.53	0.45	n/a	0.58	0.57	n/a	0.33	0.25	n/a	0.53	0.45	n/a	n/a	n/a	n/a
.⊑	5-1/2	(140)	0.73	0.69	n/a	0.57	0.48	n/a	0.59	0.57	n/a	0.38	0.29	n/a	0.57	0.48	n/a	n/a	n/a	n/a
	5-7/8	(149)	0.75	0.70	0.67	0.60	0.50	0.45	0.59	0.58	0.57	0.42	0.32	0.26	0.60	0.50	0.45	n/a	n/a	n/a
ss (	6	(152)	0.75	0.70	0.67	0.61	0.51	0.45	0.59	0.58	0.57	0.43	0.33	0.27	0.61	0.51	0.45	n/a	n/a	n/a
áne	6-1/4	(159)	0.76	0.71	0.68	0.63	0.53	0.47	0.60	0.58	0.57	0.46	0.35	0.29	0.63	0.53	0.47	0.63	n/a	n/a
hid	7	(178)	0.80	0.74	0.70	0.71	0.57	0.50	0.61	0.59	0.58	0.54	0.42	0.34	0.71	0.57	0.50	0.67	n/a	n/a
tet	7-1/2	(191)	0.82	0.75	0.71	0.76	0.61	0.53	0.62	0.60	0.59	0.60	0.46	0.38	0.76	0.61	0.53	0.69	0.63	n/a
lcre	8	(203)	0.84	0.77	0.73	0.81	0.65	0.55	0.63	0.61	0.59	0.66	0.51	0.41	0.81	0.65	0.55	0.71	0.65	n/a
õ	8-7/8	(225)	0.88	0.80	0.75	0.90	0.72	0.60	0.64	0.62	0.60	077	0.60	0.48	0.90	0.72	0.60	0.75	0.69	0.64
/ ( <sup>e</sup>	9	(229)	0.88	0.80	0.75	0.91	0.73	0.61	0.64	0.62	0.60	0.79	0.61	0.49	0.91	0.73	0.61	0.75	0.69	0.65
e (c	10	(254)	0.92	0.84	0.78	1.00	0.81	0.68	0.66	0.63	0.62	0.92	0.71	0.58	1.00	0.81	0.68	0.79	0.73	0.68
anc	11	(279)	0.97	0.87	0.81	1.00	0.89	0.75	0.67	0.65	0.63	1.00	0.82	0.67	1.00	0.89	0.75	0.83	0.77	0.71
dist	12	(305)	1.00	0.91	0.84		0.97	0.81	0.69	0.66	0.64		0.94	0.76		0.97	0.81	0.87	0.80	0.75
ge	14	(356)	1.00	0.97	0.90		1.00	0.95	0.72	0.69	0.66		1.00	0.96		1.00	0.96	0.94	0.86	0.80
/ eq	16	(406)	1.00	1.00	0.95			1.00	0.75	0.71	0.69			1.00			1.00	1.00	0.92	0.86
(s)	18	(457)			1.00				0.78	0.74	0.71								0.98	0.91
Spacing (s) / edge distance (c_a) / concrete thickness (h),	20	(508)							0.82	0.77	0.73								1.00	0.96
pac	24	(610)							0.88	0.82	0.78									1.00
S	30	(762)							0.97	0.90	0.85						İ			
	36	(914)							1.00	0.98	0.92						İ			
	> 48	(1219)								1.00	1.00						İ			

### Table 8 — Load adjustment factors for M16, M20, and M24 Hilti HSL4 anchors in uncracked concrete <sup>1,2</sup>

#### Table 9 — Load adjustment factors for M8, M10, and M12 Hilti HSL4 anchors in cracked concrete<sup>1,2</sup>

			Spac	ing fac	tor in	Edc	e dista	nce	Spac	ing fac	tor in		Edg	e distar	nce in s		from	Concr	ete thic	kness
	, M20 and M cracked con			tension			or in ter			shear <sup>3</sup>		То	⊥_ ward ec	lao	ii to a	nd awa edge	y from	i i	factor shear	4
		01010		f <sub>AN</sub>			∫ <sub>RN</sub>			f <sub>AV</sub>		101	$f_{\rm RV}$	iye		$f_{\rm RV}$			$f_{\rm HV}$	
	Nominal d	ia.	M16	M20	M24	M16	M20	M24	M16	M20	M24	M16	M20	M24	M16	M20	M24	M16	M20	M24
E	ffective	in.	3.948	4.92	5.91	3.948	4.92	5.91	3.948	4.92	5.91	3.948	4.92	5.91	3.948	4.92	5.91	3.948	4.92	5.91
emb	edment h <sub>ef</sub>	(mm)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)	(100)	(125)	(150)
	4	(102)	0.67	n/a	n/a	n/a	n/a	n/a	0.55	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a
	4-1/2	(114)	0.69	n/a	n/a	n/a	n/a	n/a	0.56	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a
Ê	4-3/4	(121)	0.70	n/a	n/a	0.85	n/a	n/a	0.56	n/a	n/a	0.22	n/a	n/a	0.43	n/a	n/a	n/a	n/a	n/a
(mm)	5	(127)	0.71	0.67	n/a	0.88	0.76	n/a	0.56	0.55	n/a	0.23	0.18	n/a	0.47	0.36	n/a	n/a	n/a	n/a
.⊑	5-1/2	(140)	0.73	0.69	n/a	0.95	0.81	n/a	0.57	0.56	n/a	0.27	0.21	n/a	0.54	0.42	n/a	n/a	n/a	n/a
	5-7/8	(149)	0.75	0.70	0.67	1.00	0.84	0.75	0.57	0.56	0.55	0.30	0.23	0.19	0.59	0.46	0.37	n/a	n/a	n/a
SS	6	(152)	0.75	0.70	0.67	1.00	0.86	0.76	0.58	0.56	0.56	0.31	0.24	0.19	0.61	0.47	0.38	n/a	n/a	n/a
kne	6-1/4	(159)	0.76	0.71	0.68	1.00	0.88	0.78	0.58	0.57	0.56	0.33	0.25	0.20	0.65	0.50	0.41	0.56	n/a	n/a
thic	7	(178)	0.80	0.74	0.70	1.00	0.96	0.84	0.59	0.57	0.56	0.39	0.30	0.24	0.77	0.60	0.48	0.59	n/a	n/a
ete	7-1/2	(191)	0.82	0.75	0.71	1.00	1.00	0.88	0.59	0.58	0.57	0.43	0.33	0.27	0.86	0.66	0.54	0.62	0.56	n/a
ncre	8	(203)	0.84	0.77	0.73	1.00	1.00	0.92	0.60	0.59	0.57	0.47	0.36	0.30	0.94	0.73	0.59	0.64	0.58	n/a
Ö	8-7/8	(225)	0.88	0.80	0.75	1.00	1.00	1.00	0.61	0.59	0.58	0.55	0.43	0.35	1.00	0.85	0.69	0.67	0.61	0.57
$c_{a})/c$	9	(229)	0.88	0.80	0.75	1.00	1.00	1.00	0.61	0.60	0.58	0.56	0.43	0.35	1.00	0.87	0.71	0.67	0.62	0.58
edge distance (c_) / concrete thickness (h),	10	(254)	0.92	0.84	0.78	1.00	1.00	1.00	0.63	0.61	0.59	0.66	0.51	0.41	1.00	1.00	0.83	0.71	0.65	0.61
tano	11	(279)	0.97	0.87	0.81	1.00	1.00	1.00	0.64	0.62	0.60	0.76	0.59	0.48	1.00	1.00	0.95	0.75	0.68	0.64
dis	12	(305)	1.00	0.91	0.84		1.00	1.00	0.65	0.63	0.61	0.87	0.67	0.54		1.00	1.00	0.78	0.71	0.67
dge	14	(356)	1.00	0.97	0.90			1.00	0.68	0.65	0.63	1.00	0.84	0.68			1.00	0.84	0.77	0.72
	16	(406)	1.00	1.00	0.95				0.70	0.67	0.65		1.00	0.84				0.90	0.82	0.77
(s)	18	(457)			1.00				0.73	0.69	0.67			1.00				0.95	0.87	0.82
sing	20	(508)							0.75	0.71	0.68			1.00				1.00	0.92	0.86
Spacing (s)	24	(610)							0.80	0.76	0.72								1.00	0.94
S	30	(762)							0.88	0.82	0.78									1.00
	36	(914)							0.95	0.88	0.83									
	> 48	(1219)							1.00	1.00	0.94									Í

1. Linear interpolation not permitted.

2. When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Engineering software or perform anchor calculation using design equations from ACI 318 Chapter 17.

3. Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AV}$ . 4. Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ . If a reduction factor value is in a shaded cell, it may not be permitted if both edge and spacing are less than "critical" distances. Check table 5 and figure 2 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. For the HSL4-SH M8, M10 and M12 diameters, the minimum slab thickness must be increased by 5 mm (3/16-in.).

Anchor Fastening Technical Guide Edition 21 | 3.0 ANCHORING SYSTEMS | 3.3.2 HSL4 HEAVY-DUTY EXPANSION ANCHORS Hilti, Inc. 1-800-879-8000 | en español 1-800-879-5000 | www.hilti.com | Hilti (Canada) Corporation | www.hilti.ca | 1-800-363-4458

## DESIGN INFORMATION IN CONCRETE PER CSA A23.3

Limit State Design of anchors is described in the provisions of CSA A23.3 Annex D for post-installed anchors tested and assessed in accordance with ACI 355.2 for mechanical anchors and ACI 355.4 for adhesive anchors. This section contains the Limit State Design tables with unfactored characteristic loads that are based on the published loads in ICC Evaluation Services ESR-4386. These tables are followed by factored resistance tables. The factored resistance tables have characteristic design loads that are prefactored by the applicable reduction factors for a single anchor with no anchorto-anchor spacing or edge distance adjustments for the convenience of the user of this document. All the figures in the previous ACI 318 Chapter 17 design section are applicable to Limit State Design and the tables will reference these figures.

For a detailed explanation of the tables developed in accordance with CSA A23.3 Annex D, refer to PTG Ed. 21 Section 3.1.8. Technical assistance is available by contacting Hilti Canada at (800) 363-4458 or at www.hilti.com.

	- Sleer Slier			157		*
	HSL	.4, HSL4-B, HSL4	1-SK		HSL4-G	
Nominal anchor diameter	Tensile³ φN <sub>sa</sub> Ib (kN)	Shear⁴ φV <sub>sa</sub> Ib (kN)	Seismic shear <sup>5</sup> ¢V <sub>sa,eq</sub> Ib (kN)	Tensile³ φN <sub>sa</sub> Ib (kN)	Shear <sup>4</sup> φV <sub>sa</sub> Ib (kN)	Seismic shear <sup>5</sup> $\varphi V_{_{sa,eq}}$ Ib (kN)
M8	4,495	4,615	2,940	4,495	3,870	2,410
	(20.0)	(20.5)	(13.1)	(20.0)	(17.2)	(10.7)
M10	7,100	6,520	5,390	7,100	5,345	4,415
	(31.6)	(29.0)	(24.0)	(31.6)	(23.8)	(19.6)
M12	10,335	9,385	7,580	10.335	7,755	6,265
	(46.0)	(41.7)	(33.7)	(46.0)	(34.5)	(27.9)
M16	19,170	17,025	15,805	19,170	14,460	13,430
	(94 .0)	(75.7)	(70.3)	(85.3)	(64.3)	(59.7)
M20	29,975	25,195	18,575	29,975	21,140	15,595
	(133.3)	(112.1)	(82.6)	(133.3)	(94.0)	(69.4)
M24	43,145 (191.9)	29,295 (130.3)	24,335 (108.2)	43,145 (191.0)	27,520 (122.4)	n/a

## Table 10 — Steel strength for Hilti HSL4 anchors<sup>1,2</sup>

1. See PTG Ed. 21 section 3.1.8 to convert design strength value to ASD value.

2. Hilti HSL4 anchors are to be considered ductile steel elements.

3. Tensile  $N_{sar}$  =  $A_{se,}N$   $\varphi_{s}$   $f_{uta}$  R as noted in CSA A23.3 Annex D .

4. Shear determined by static shear tests with  $V_{sar}$  <  $A_{se,V}$   $\varphi_s$  0 .6  $f_{uta}$  R as noted in CSA A23.3 Annex D .

5. Seismic shear values determined by seismic shear tests with  $V_{sareq}$  < Ase, V  $\varphi_s$  0 .6  $f_{uta}$  R as noted in CSA A23.3 Annex D . See Section 3.1.8 for additional information on seismic applications.

### Table 11 — Hilti HSL4 design information in accordance with CSA A23.3 Annex D<sup>1</sup>

3.3.2

			Nominal anchor diameter						
Design parameter	Symbol	Units	M8	M10	M12	M16	M20	M24	Ref A23.3
Anchor O.D.	d <sub>a</sub>	mm (in.)	12 (0.47)	15 (0.59)	18 (0.71)	21 (0.94)	28 (1.10)	32 (1.26)	
Effective minimum embedment <sup>2</sup>	h <sub>ef</sub>	mm (in.)	60 (2.4)	70 (2.8)	80 (3.1)	100 (3.9)	125 (4.9)	150 (5.9)	
Minimum concrete thickness	h <sub>min</sub>	mm (in.)	See table 5						
Critical edge distance	C <sub>ac</sub>	mm (in.)	See table 5						
Minimum edge distance		mm (in.)	See table 5						
		mm (in.)	See table 5						
Minimum anchor spacing		mm (in.)	See table 5						
		mm (in.)	See table 5						
Minimum hole depth in concrete	h <sub>o</sub>	mm (in.)	80 (3.1)	90 (3.5)	105 (4.1)	125 (4.9)	155 (6.1)	190 (7.5)	
Minimum specified yield strength	f <sub>ya</sub>	N/mm <sup>2</sup> (psi)			64 (93,	41 000)			
Minimum specified ultimate strength	f <sub>uta</sub>	N/mm <sup>2</sup> (psi)	800 (116,000)						
Effective tensile stress area	A <sub>se,N</sub>	mm <sup>2</sup> (in <sup>2</sup> )	36.8 (0.057)	58.1 (0.090)	84.5 (0.131)	156.8 (0.243)	245.2 (0.380)	352.9 (0.547)	
Steel embed. material resistance factor for reinforcement	φ.	-	0.85					8.4.3	
Resistance modification factor for tension, steel failure modes <sup>3</sup>	R	-	0.80					D.5.3	
Resistance modification factor for shear, steel failure modes <sup>3</sup>	R	-	0.75					D.5.3	
Factored steel resistance in tension	N <sub>sar</sub>	lb (kN)	4,495 (20.0)	7,100 (31.6)	10,335 (46.0)	19,170 (85.3)	29,975 (133.3)	43,145 (191.9)	D.6.1.2
Factored steel resistance in shear HSL4, HSL-B, HSL4-SK		lb (kN)	4,615 (20.5)	6,520 (29.0)	9,385 (41.7)	17,025 (75.7)	25,195 (112.1)	29,295 (130.3)	D.7.1.2
Factored steel resistance in shear HSL4-G	V <sub>sar</sub>	lb (kN)	3,870 (17.2)	5,345 (23.8)	7,755 (34.5)	14,460 (62.3)	21,140 (94.0)	27,520 (122.4)	D.7.1.2
Factored steel resistance in shear, seismic HSL4, HSL-B, HSL4-SK		lb (kN)	2,940 (13.1)	5,390 (24.0)	7,580 (33.7)	15,805 (70.3)	18,575 (82.6)	24,335 (108.3)	
Factored steel resistance in shear, seismic HSL4-G	- V <sub>sar,eq</sub>	lb (kN)	2,410 (10.7)	4,415 (19.6)	6,265 (27.9)	13,430 (59.7)	15,595 (69.4)	n/a <sup>7</sup>	
Coeff. for factored conc. breakout resistance, uncracked concrete	k <sub>c,uncr</sub>	-	10				D.6.2.2		
Coeff. for factored conc. breakout resistance, cracked concrete	k <sub>c,cr</sub>	-	7 10					D.6.2.2	
Modification factor for anchor resistance, tension, uncracked concrete <sup>4</sup>	Ψ <sub>c,N</sub>	_	1.0					D.6.2.6	
Anchor category	-	-	1.0					D.5.3(c)	
Concrete material resistance factor	φ.	-	0.65					8.4.2	
Resistance modification factor for tension and shear, concrete failure modes, Condition B <sup>5</sup>	R	-	1.0					D.5.3(c)	
Factored pullout resistance in 20 MPa uncracked concrete <sup>6</sup>	N <sub>pr,uncr</sub>	lb (kN)	2,945 (13.1)	n/a	n/a	n/a	n/a	n/a	D.6.3.2
Factored pullout resistance in 20 MPa cracked concrete <sup>6</sup>	N <sub>pr,cr</sub>	lb (kN)	1,970 (8.8)	3,150 (14.0)	n/a	n/a	n/a	n/a	D.6.3.2
Factored seismic pullout resistance in 20 MPa cracked concrete <sup>6</sup>	N <sub>pr,eq</sub>	lb (kN)	1,970 (8.8)	3,150 (14.0)	n/a	n/a	n/a	10,030 <sup>7</sup> (44.6)	
Load bearing length of anchor in shear	l <sub>e</sub>	mm (in.)	24 (0.94)	30 (0.94)	30 (1.18)	36 (1.42)	56 (2.20)	64 (2.52)	D.7.2.2

Design information in this table is taken from ICC-ES ESR-4386, table 3, and converted for use with CSA A23.3 Annex D. 1

2 3 4 See Figure 1 of this document.

The HSL4 is considered a ductile steel element as defined by CSA A23.3 Annex D section D.2. For all design cases,  $\psi_{e,N} = 1.0$ . The appropriate coefficient for breakout resistance for cracked concrete ( $k_{e,or}$ ) or uncracked concrete ( $k_{e,oro}$ ) must be used . For use with the load combinations of CSA A23.3 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 section D.5.3 is not provided, or 5 where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used. 6 For all design cases,  $\psi_{e,P} = 1.0$ . NA (not applicable) denotes that this value does not control for design. See section 4.1.4 of ESR-4386 for additional information.

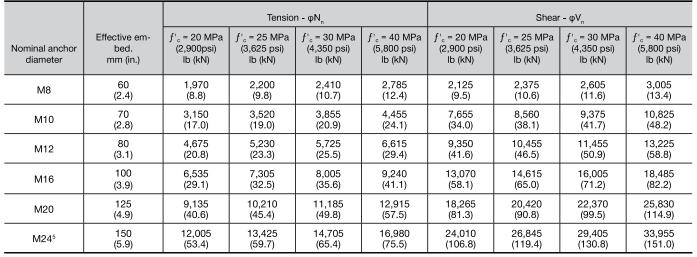
7 HSL4-G M24 is not permitted for seismic applications.



		Tension - φN <sub>n</sub>			Shear - φV <sub>n</sub>				
Nominal anchor diameter	Effective em- bed. mm (in.)	f' <sub>c</sub> = 20 MPa (2,900psi) Ib (kN)	f' <sub>c</sub> = 25 MPa (3,625 psi) Ib (kN)	f' <sub>c</sub> = 30 MPa (4,350 psi) Ib (kN)	f' <sub>c</sub> = 40 MPa (5,800 psi) Ib (kN)	f' <sub>c</sub> = 20 MPa (2,900 psi) Ib (kN)	f' <sub>c</sub> = 25 MPa (3,625 psi) Ib (kN)	f' <sub>c</sub> = 30 MPa (4,350 psi) Ib (kN)	f' <sub>c</sub> = 40 MPa (5,800 psi) Ib (kN)
M8	60	2,945	3,290	3,605	4,165	3,035	3,395	3,720	4,295
	(2.4)	(13.1)	(14.6)	(16.0)	(18.5)	(13.5)	(15.1)	(16.5)	(19.1)
M10	70	3,825	4,280	4,685	5,415	7,655	8,560	9,375	10,825
	(2.8)	(17.0)	(19.0)	(20.9)	(24.1)	(34.0)	(38.1)	(41.7)	(48.2)
M12	80	4,675	5,230	5,725	6,615	9,350	10,455	11,455	13,225
	(3.1)	(20.8)	(23.3)	(25.5)	(29.4)	(41.6)	(46.5)	(50.9)	(58.8)
M16	100	6,535	7,305	8,005	9,240	13,070	14,615	16,005	18,485
	(3.9)	(29.1)	(32.5)	(35.6)	(41.1)	(58.1)	(65.0)	(71.2)	(82.2)
M20	125	9,135	10,210	11,185	12,915	18,265	20,420	22,370	25,830
	(4.9)	(40.6)	(45.4)	(49.8)	(57.5)	(81.3)	(90.8)	(99.5)	(114.9)
M24	150	12,005	13,425	14,705	16,980	24,010	26,845	29,405	33,955
	(5.9)	(53.4)	(59.7)	(65.4)	(75.5)	(106.8)	(119.4)	(130.8)	(151.0)

## Table 12 — Hilti HSL4 anchors factored resistance with concrete/pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>

## Table 13 — Hilti HSL4 anchor factored resistance with concrete / pullout failure in cracked concrete<sup>1,2,3,4,5</sup>



1 See PTG Ed. 21 section 3.1.8 to convert design strength value to ASD value.

2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

3 Apply spacing, edge distance, and concrete thickness factors in tables 6 to 9 as necessary. Compare to the steel values in table 10. The lesser of the values is to be used for the design. 4 Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: for sand-lightweight,  $\lambda_a = 0.68$ ; for all-lightweight,

4 Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ<sub>a</sub> as follows: for sand-lightweight, λ<sub>a</sub> = 0.68; for λ<sub>a</sub> = 0.60

5 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic tension loads, multiply cracked concrete tabular values in tension only by the following reduction factors:

M24 -  $\alpha_{N,seis}$  = 0 .62. HSL4-G M24 is not permitted for seismic applications.

All other sizes -  $\alpha_{N,seis} = 0.75$ 

No reduction needed for seismic shear. See PTG Ed. 21 section 3.1.8 for additional information on seismic applications.

## INSTALLATION INSTRUCTIONS

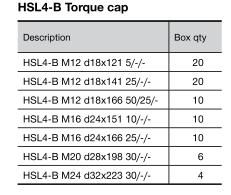
Installation Instructions For Use (IFU) are included with each product package. They can also be viewed or downloaded online at www.hilti.com. Because of the possibility of changes, always verify that downloaded IFU are current when used. Proper installation is critical to achieve full performance. Training is available on request. Contact Hilti Technical Services for applications and conditions not addressed in the IFU.

## **ORDERING INFORMATION**



## **HSL4 Bolt version**

Description	Box qty	
HSL4 M8 d12x97 20/-/-	40	
HSL4 M8 d12x117 40/20/-	40	
HSL4 M10 d15x109 20/-/-	20	
HSL4 M10 d15x129 40/20/-	20	
HSL4 M12 d18x131 25/-/-	20	
HSL4 M12 d18x156 50/25/-	20	
HSL4 M16 d24x138 10/-/-	10	
HSL4 M16 d24x153 25/-/-	10	
HSL4 M16 d24x178 50/25/-	10	
HSL4 M20 d28x183 30/-/-	6	
HSL4 M20 d28x213 60/30/-	6	
HSL4 M24 d32x205 30/-/-	4	
HSL4 M24 d32x235 60/30/-	4	





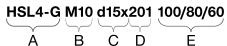
### **HSL4-G Stud version**

Description	Box qty	
HSL4-G M8 d12x107 20/-/-	40	
HSL4-G M10 d15x121 20/-/-	20	
HSL4-G M10 d15x201 100/80/60	20	
HSL4-G M12 d18x147 25/-/-	20	
HSL4-G M12 d18x172 50/25/-	20	
HSL4-G M16 d24x175 25/-/-	10	
HSL4-G M16 d24x200 50/25/-	10	
HSL4-G M20 d28x205 30/-/-	6	
HSL4-G M20 d28x235 60/30/-	6	

## HSL4-SK Countersunk

Description	Box qty
HSL4-SK M8 d12x80 10/-/-	20
HSL4-SK M8 d12x90 20/-/-	20
HSL4-SK M10 d15x100 20/-/-	10
HSL4-SK M12 d18x120 25/-/-	10

## Product nomenclature



A: Anchor Name

B: Threaded rod diameter

C: Drill bit diameter

D: Total length of the anchor

E: Maximum fixture thickness at Min/Std/Max effective embedment

Anchor Fastening Technical Guide Edition 21 | 3.0 ANCHORING SYSTEMS | 3.3.2 HSL4 HEAVY-DUTY EXPANSION ANCHORS Hilti, Inc. 1-800-879-8000 | en español 1-800-879-5000 | www.hilti.com | Hilti (Canada) Corporation | www.hilti.ca | 1-800-363-4458

3.3.2